

FOCUS ERROR CORRECTION METHOD AND APPARATUS

FIELD OF THE INVENTION

This invention is in the field of auto-focusing techniques and relates to a method and apparatus enabling focus error correction to maintain a desired position of an article.

BACKGROUND OF THE INVENTION

5 There are a number of optical systems utilizing focus error correction techniques. Such optical systems, which typically comprise an illumination system equipped with suitable light directing optics and a detection system equipped with light collecting optics, are used for inspection/measurements of articles, reading/recording information in an information carrier, etc. The focus error correction technique ensures that the article
10 under inspection (or an addressed layer of the information carrier) is located in a focal plane defined by the light directing optics.

 According to one conventional auto-focusing technique disclosed, for example, in U.S. Patent Nos. 4,123,652 and 5,563,702, a light beam scattered from an article is directed through anamorphic elements, and the shape of the light beam cross-section after
15 passing these elements is monitored. The basic principle underlying the implementation is that a cylindrical lens produces astigmatism. A focused beam is first displaced from an in-focus point in a first direction, and then in a second direction perpendicular to the first direction. The beam cross section therefore changes from being oblong in the first direction, to being circular, to being oblong in the second direction. Thus, an auto-focus
20 beam is typically split into a pair of sub-beams, which propagate along mutually perpendicular optical paths onto a pair of detectors through a pair of astigmatic elements, respectively. The detectors are quadrature photodiodes. When the article is in focus,

both detectors are illuminated by a circular beam. As the article goes out of focus, the horizontal diameter of the beam decreases on one detector and increases on the other. This changes the electrical output from the quadrature detectors and the focus correction signal is thus calculated accordingly.

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SUMMARY OF THE INVENTION

There is a need in the art to facilitate focus error correction by providing a novel method and apparatus utilizing a dynamic auto-focusing technique. The present invention enables the detection of a position of the plane defined by an article under processing relative to the focal plane of an optical system, thereby enabling maintenance of accurate focusing of an incident beam from the optical system to the article.

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The term "processing" used herein signifies any procedure applied to the article during which the article should be maintained in a preset plane. This procedure may be inspection, information reading/recording, etc.

One aspect of the present invention is based on the detection of at least two interference patterns formed by light components returned from an elongated illuminated region on the article and passing through at least two symmetrical peripheral regions of the optical axis of a focusing/collecting lens arrangement. The term "periphery regions" used herein signifies regions of light propagation along an optical axis of the lens making substantially large angles to and lying substantially far from the optical axis (as compared to paraxial regions of the optical axis).

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Each of the interference patterns is created by interference between collected light formed of light components propagating within one of the periphery regions and collected light formed of light components propagating within the paraxial regions of the optical

axis. The relation between the interference patterns is indicative of the phase difference between the collected light formed of light components propagating within the paraxial and periphery regions, and consequently, of the out-of-focus position of the illuminated region.

5 One concept underlying the present invention is based on the following known phenomena. Light waves returned from in-focus and out-of-focus planes and passed through a focusing lens have substantially flat and spherical wave fronts, respectively. Consequently, information indicative of distortions produced at any out-of-focus location is actually that contained in light propagating within a periphery region of the optical
10 axis, rather than that associated with a paraxial area. Hence, it is desired to analyze light components propagating within the periphery regions, to detect the focus error. On the other hand, light components propagating within the paraxial and periphery regions of the optical axis have different optical paths, respectively, and therefore have a certain phase difference indicative of the out-of-focus position of the article.

15 In the inventive apparatus, the same focusing optics (typically composed of one or more objective lens) directs incident light onto an elongated region of the article, and collects light returned from the illuminated elongated region. This focusing optics presents an aperture stop whose physical dimensions define the collected light portion. Collected light, which contains information of the illuminated region and of the aperture
20 stop, enters a focus detection unit, and is directed towards the sensing surface of a detector through an optical system.

When the collected light passes through the optical system, an image of the aperture stop is first created (by a first lens arrangement) in a plane conjugate to the

aperture stop plane and extending in an X-Y plane perpendicular to the optical axis of light propagation through the optical system. Then, at least three spatially separated light components are picked up (selected) from the light indicative of this image by appropriately locating at least three slits in the image plane, and are imaged onto the
5 sensing surface of the detector by suitable optics (second and third lens arrangements). The slits are accommodated such that at least one of the selected light components contains light propagated within the paraxial region of the optical axis of the focusing/collecting optics, and the at least two other light components contain light propagated within two symmetrical periphery regions of the optical axis. The slits are
10 made in a blocking plate (located in the X-Y plane), extend along the X-axis (parallel to the elongated illuminated region), and are aligned in a spaced-apart parallel relationship along the Y-axis, such that the optical axis of the optical system intersects with an axis of the at least one central slit.

The central slit may be relatively long, extending across the entire blocking plate,
15 or may be in the form of a two-part slit, the two parts being spaced apart from each other along the X-axis and being spaced from at least two side slits along the Y-axis. The side slits may be relatively short (as compared to the long central slit). The side slit(s) located at opposite sides of the central slit are centrally symmetrical relative to the intersection point between the slits' plane and the optical axis of the optical system, and are spaced
20 from each other along both the X- and Y-axes.

According to one embodiment of the invention, there are provided two side slits located at opposite sides of the central slit. In this case, two interference patterns are created.

According to another embodiment of the invention, two pairs of side slits are located at respective opposite sides of the central slit. In this manner, a dynamic range of the detected signals can be extended. The slits of each pair may be spaced from each other along the Y-axis only, in which case two interference patterns are created, or may
5 be spaced from each other along both the X- and Y-axis, in which case two pairs of interference patterns are created.

The slits are sufficiently thin to cause the diffraction of light emerging from the slits. Two interference patterns are created on the sensing surface by the interference between, respectively, the diffracted light ensuing from the upper slit(s) and the
10 respective half (or part) of the central slit, and the diffracted light ensuing from the lower slit(s) and the other half (or part) of the central slit.

When the article is in focus, the two patterns are spaced from each other only along the X-axis, namely each two corresponding "dark" fringes and each two corresponding "light" fringes in the patterns are aligned in two lines, respectively. This is
15 the so-called "best focus image".

When the article goes out of focus, the optical paths of the collected light components change, and, consequently, a phase difference is created between the light components emerging from the central and upper slits, as well as between the central and the lower slits. This causes the interference pattern to move up and down on the sensing
20 surface of the detector. The two imaged interference patterns are formed by light components propagating symmetrically with respect to the optical axis. Therefore, images corresponding to the before-focus and after-focus locations of the illuminated region (line) displace into two opposite directions, respectively, relative to the "best focus

image". In other words, when one interference pattern moves up, the other pattern moves down and vice versa. By estimating the phase difference between the two patterns, the focus error can be estimated.

By equipping the apparatus with a feedback loop, typically consisting of a suitable
5 processor interconnected between an output circuit of the detector and a servomotor coupled to the article support stage or/and to the focusing optics, it is possible to perform focus error correction successfully.

There is thus provided, according to one aspect of the present invention, an optical
apparatus for determining a position of an article, the apparatus comprising an
10 illumination unit, focusing optics and a focus detection unit, wherein:

the illumination unit is operable to generate incident light and illuminate an
elongated region of the article for producing light returned from the
illuminated region;

the focusing optics directs the incident light toward the article and directs at least a
15 portion of the returned light towards the focus detection unit; and

the focus detection unit comprises an optical system and a detector, the optical
system being operable to collect the directed portion of the returned light
and create at least two images on a sensing surface of the detector in the
form of at least two interference patterns, respectively, wherein at least one
20 pattern is created by interference between light components of the
collected light that propagated within a first periphery region of an optical
axis of the focusing optics and light components of the collected light that
propagated within a paraxial region of said optical axis, and at least one

other interference pattern is created by interference between light components of the collected light that propagated within a second periphery region of said optical axis, substantially symmetrical to said first periphery region with respect to said optical axis, and light components of the collected light that propagated within the paraxial region of said optical axis, data representative of a relation between intensity profiles in the at least two interference patterns being indicative of the position of the article relative to a focal plane of said focusing optics.

According to another aspect of the present invention, there is provided a focus error detection method comprising:

- passing incident light through focusing optics and illuminating an elongated region, thereby producing light returned from the illuminated region;
- collecting at least a portion of the light returned from said illuminated region and passed through said focusing optics;
- picking up at least three spatially separated light components of the collected returned light, to cause diffraction of each of said light components and to allow interference between a central light component that propagated within a paraxial region of an optical axis of the focusing optics and at least one first light component that propagated within a first periphery region of said optical axis of the focusing optics, and interference between said central light component and at least one second light component of the collected returned light that propagated within a second periphery

region of said optical axis of the focusing optics substantially symmetrical to said first periphery region with respect to said optical axis; and

- creating at least two images in the form of at least two interference patterns, respectively, on a sensing surface of a detector, said at least two interference patterns being created by the interference of the separated light components, a relation between intensity profiles in the interference patterns being indicative of the position of the illuminated region relative to a focal plane of said focusing optics.

5 The present invention may be used with an optical inspection system, by simply adding a separate detection-collection means for collecting light returned from the illuminated region at elevation angles other than that collected by the focusing optics. There is no need for a separate illumination unit, though one may be provided if desired.

Thus, according to yet another aspect of the present invention, there is provided a system for an optical inspection of an article, comprising an optical apparatus for maintaining a desired position of the article, and at least one detection unit, wherein said optical apparatus comprises:

- an illumination unit operable to generate incident light and illuminate an elongated region of the article for producing light returned from the illuminated region;
- 20 focusing optics that directs the incident light towards the article and directs at least a portion of the returned light towards a focus detection unit;
- said focus detection unit comprising an optical system and a detector, the optical system being operable to collect the directed portion of the returned light

and create at least two images on a sensing surface of the detector in the form of at least two interference patterns, respectively, wherein at least one pattern is created by interference between light components of the collected light that propagated within a first periphery region of an optical axis of the focusing optics and light components of the collected light that propagated within a paraxial region of said optical axis, and at least one other interference pattern is formed by interference between light components of the collected light that propagated within a second periphery region of said optical axis, substantially symmetrical to said first periphery region with respect to said optical axis, and light components of the collected light that propagated within the paraxial region of said optical axis of the focusing optics, data indicative of a relation between intensity profiles in the at least two interference patterns being indicative of the position of the article relative to a focal plane of the focusing optics; and

15 said at least one detection unit comprises a light collecting optics and a detection means, the light collecting optics being capable of collecting light returned from the article at elevation angles different from an elevation angle of collection of said at least portion of the returned light defined by said focusing optics.

20 According to yet another aspect of the present invention, there is provided a method of maintaining a desired position of an article during processing of the article, the method comprising:

- 5 (a) generating an incident beam and illuminating an elongated region of the article to produce light returned from the illuminated region;
- (b) directing the incident light towards the article through a focusing optics, and collecting with said focusing optics at least a portion of the returned light and directing it towards a focus detection unit, said focusing optics defining an aperture stop of light collection;
- 10 (c) creating from the collected returned light at least two images of the illuminated region in the form of at least two interference patterns, respectively, said at least two interference patterns being formed by the interference between a central light component of the collected light that propagated within a paraxial region of an optical axis of the focusing optics and at least one first light component of the collected light that propagated within a first periphery region of the optical axis of the focusing optics, and interference between said central light component and
- 15 at least one second light component of the collected light that propagated within a second periphery region of the optical axis of the focusing optics substantially symmetrical to said first periphery region with respect to said optical axis;
- (d) detecting light indicative of said at least two images and generating data representative thereof; and
- 20 (e) analyzing the generated data to determine a relation between intensity profiles in the at least two interference patterns, and determining a relative

position of the article with respect to a focal plane of the focusing optics,
thereby enabling maintenance of the desired position of the article.

One embodiment of the present invention may be used with an optical inspection
system for inspecting wafers, and is therefore described as such below, by way of an
5 exemplary implementation. It is within the contemplation of the invention to provide
other implementations as well, involving systems for inspecting other kinds of articles,
including other nontranslucent articles, or reticles.

BRIEF DESCRIPTION OF THE DRAWINGS

In order to understand the invention and to see how it may be carried out in
10 practice, a preferred embodiment will now be described, by way of non-limiting example
only, with reference to the accompanying drawings, in which:

Fig. 1 is a schematic illustration of the main components of an article inspection
system utilizing an apparatus according to the invention;

Fig. 2 schematically illustrates the main constructional elements of a focus
15 detection unit of the apparatus of Fig. 1 utilizing a blocking plate according to one
example of the invention;

Figs. 3a and 3b illustrate the main principles underlying the implementation of an
auto-focusing technique in the unit of Fig. 2;

Fig. 4 illustrates an image obtained with the focus detection unit of Fig. 2
20 corresponding to the in-focus position of the article;

Figs. 5a and 5b illustrate, respectively, the entire image obtained with the focus
detection unit, and a corresponding graph representative of the output signal of a detector,
which correspond to one out-of-focus position of the article;

Figs. 6a and 6b illustrate, respectively, the entire image obtained with the focus detection unit, and a corresponding graph representative of the output signal of the detector, which correspond to another out-of-focus position of the article;

Fig. 7 more specifically illustrates the light propagation through the optical system of Fig. 2 considered for the calculation of the light intensity on a detector plane;

Figs. 8a and 8b illustrate another possible example of a blocking plate suitable for use in the focus detection unit of Fig. 2; and

Figs. 9a and 9b illustrate yet another possible example of a blocking plate suitable for use in the focus detection unit of Fig. 2.

10 **DETAILED DESCRIPTION OF A PREFERRED EMBODIMENT**

Fig. 1 shows an optical inspection system 1 associated with a wafer 2 to be inspected. The wafer 2 is typically located on a support stage 3 which translates the wafer within an inspection plane. The system 1 comprises a scanning apparatus 1a defining an auto-focusing channel, and bright-field and dark-field detection units 1b and 1c associated with inspection channels. The construction and operation of the detection units 1b and 1c are known, and therefore need not be specifically described, except to note the following. The dark-field detection unit 1c comprises a suitable detector and appropriately oriented collecting optics. The bright field detection unit 1b includes a pin-diode (not shown) receiving a part of returned radiation collected with the scanning apparatus 1a. It should be understood that, generally, either a bright-field inspection channel or a dark-field inspection channel, or both, could be used for inspection purposes.

The scanning apparatus 1a comprises an illumination unit 4, focusing-collecting optics 6, and a focus detection unit 8. The unit 8 comprises an optical system 9 and a

detector 10 together constituting the auto-focusing channel, the construction and operation of which will be described more specifically further below with reference to Fig. 2.

5 A beam splitter 11 separates the incident and returned radiation, and directs the returned radiation towards the optical system 9. According to the present example, the beam splitter 11 is in the form of a partially transparent mirror that transmits and reflects radiation impinging thereon from two opposite directions, respectively. The beam splitter 11 transmits incident radiation and reflects returned radiation. Alternatively, a polarizing beam splitter equipped with phase-shifting plates may be used.

10 The illumination unit 4 comprises a laser source 12 emitting an incident beam 14, and a deflector 15 (which may be an acousto-optic element, a mirror, or the like) causing the beam 14 to scan along a surface 2a of the wafer 2. It should be noted that a linear beam could be used for the same purpose, i.e., for illuminating an elongated region on the surface 2a.

15 The focusing-collecting optics 6 is typically an objective lens system 16 (which could be one or a plurality of objective lenses). The objective lens system 16 focuses the deflected beam 14 onto a scan line S (constituting the elongated region) on the surface 2a, and collects a portion of the returned light.

20 A servomotor 18 is coupled to the stage 3 for driving a movement of the stage along an optical axis OA1 of the lens system 16 to change the position of its focal plane P relative to the surface 2a. Alternatively or additionally, a similar servomotor may be associated with the part or all of illumination unit 4, or the lens system 16. Relative

movement between the surface 2a and the beam 14, however achieved to effect scanning is within the contemplation of the invention.

The detector 10 comprises a charge coupled device (CCD) camera 20 having a plurality of sensing elements (not shown) that typically detect light signals and generate
5 electrical output representative thereof to be transmitted through an output circuit 22 of the detector. The sensing elements define together a sensing surface 21 (shown schematically in Fig. 2).

Interconnected between the servomotor 18 and the output circuit 22 is a processor 24. The construction and operational principles of the processor 24 may be of any known
10 kind. However, it should be noted that the processor 24 is responsive to the output of the detection unit 10 for analyzing the location of the surface 2a relative to the focal plane P and generating a focus error correction signal, upon detecting that the surface 2a moves away from the focal plane P. Thus, the CCD output circuit 22, processor 24 and servomotor 18 constitute together a feedback loop. The processor 24 is optionally
15 provided with a display 26 for displaying obtained images.

Also provided in the system 1 is a beam splitter 27 accommodated in the optical path of the collected returned light reflected from the mirror 11. The beam splitter 27 is a semi-transparent mirror that partly transmits and partly reflects radiation impinging thereon. Hence, the mirror 27 reflects a part of the collected radiation towards the
20 detection unit 1b, while transmitting the other part of the collected radiation towards the focus detection unit 8.

The incident beam 14 propagates through the beam splitter 11 and objective lens 16, and illuminates the line S, while being focused onto the focal plane P, which

occasionally may not coincide with the surface 2a. The beams' propagation is shown here schematically to facilitate the illustration of the main components and operational principles of the apparatus 1a. A light portion, generally at 28, returned (reflected) from the scan line S, is collected by the lens system 16. The lens system 16 may include an aperture stop that defines the collected light portion 28. The collected light 28 is reflected to the mirror 27, which allows the transmission of the part of light 28 towards the detector 10 through the optical system 9, and reflects the other part of light 28 towards the detection unit 1b. The optical system 9 forms images indicative of the position of the surface 2a relative to the focal plane P on the sensing surface 21.

Fig. 2 shows more detail of the construction of one implementation of the focus detection unit 8. The optical system 9 comprises three functionally different lens arrangements, generally designated 30, 32 and 34, respectively, and a blocking plate 35 interposed between the lens arrangements 30 and 32. The lens arrangements define a common optical axis OA_2 of light propagation through the optical system 9. The plate 35 is oriented perpendicularly to the optical axis OA_2 , i.e., in the X-Y plane.

The plate 35 is formed with three slits 35a, 35b and 35c aligned in a spaced-apart parallel relationship along the Y-axis, the slits 35a and 35b being also spaced with respect to each other along the X-axis. A different number of slits may be desired, depending on the application. The slits may be considered thin, being about $5\mu\text{m}$ wide. The three slits represent three transmitting regions, respectively, surrounded by blocking regions of the plate 35, thereby picking up three light components from light impinging onto the plate 35 and transmitting them towards the lens arrangement 32. The central slit 35b may extend substantially across the entire plate 35. In this embodiment, the upper and lower

slits 35a and 35c are short (as compared to the central slit) and are located centrally symmetrically relative to an intersection point IP_1 between the plate 35 and the optical axis OA_2 . The purpose of such a slit arrangement will be explained further below.

The back reflected light 28 is directed by the beam splitter 11 towards the lens arrangement 30. The lens arrangement 30 comprises two lenses 36 and 38 with focal lengths of 200mm and 80mm, respectively, spaced from each other a distance d_1 ($d_1=280\text{mm}$). Obviously, other lenses with different focal lengths and spacings may be used. It should also be noted that the illustration is schematic, and does not proportionally correspond to the actual distances between the elements of the unit 8, in order to facilitate the illustration of some elements of the system, such as plate 35 and sensing surface 21 of the camera. The lenses 36 and 38 operate together to image the aperture stop 16 onto a slits' plane CP_1 . That is, lenses 36 and 38 operate in a telescopic mode to form a magnified image of the aperture stop 16 in the plane CP_1 . A plane CP_0 , defined by the location of the aperture stop 16 ("object"), and the slits' plane CP_1 are conjugate planes, i.e., are the images of each other.

The image magnification is required to adapt the exit pupil size (i.e., the size of the aperture stop 16) to the target size (i.e., the sensing surface 21 of the CCD camera 20). As shown in the figure, S' is an image of the scan line S formed by the lens 36. Generally speaking, the arrangement 30, in combination with the beam splitter 11, represents a translation matrix to move image formation away from optical interfaces defined by the focusing optics 6.

The plate 35 is accommodated within the conjugate plane CP_1 at the location of the expected magnified image of the aperture stop 16. Since light impinging onto the

plate 35 is the "image" of the aperture stop 16, it contains the same information of the out-of-focus distortions as the "object" light 28 impinging onto the aperture stop 16. Light coming from the plate 35 is in the form of three spatially separated light components 28a, 28b and 28c representative of the image of the aperture stop 16.

5 The lens arrangement 32 consists of a spherical lens 40 (or a plurality of such lenses), that forms an image of the scan line S along the Z-axis in its focal plane. The lens 40, which in this embodiment has a 200mm focal length and is located in the focal plane of the lens 38, i.e., is spaced from lens 38 a distance d_2 equal to 80mm. The lens arrangement 32 and the CCD camera 20 are accommodated such that the sensing surface
10 21 of the camera is located in a focal plane CP_2 of the lens arrangement 32 conjugate to the plane CP_0 along the X-axis (i.e. parallel to the scan line S). Obviously other lenses with different focal lengths and spacings may be used.

 The lens arrangement 34 comprises an appropriate number of cylindrical lenses - two in the present example - designated respectively 42 and 44, which operate together to
15 form an image of the slits in the plane CP_2 . The slits' image along the X-axis is magnified in order to be projected onto the entire sensing surface 21. Each of the lenses 42 and 44 has a 50mm focal length. Lens 42 is spaced from lens 40 a distance d_3 equal to 50mm, and from lens 44 a distance d_4 equal to 100mm. Again, different numbers of lenses, with different focal lengths and spacings, may be used.

20 Figs. 3a and 3b illustrate principles of light propagation from in-focus and out-of-focus positions, underlying the above design of the optical system 9. Fig. 3a illustrates a wave front W_1 of returned light 28 passed through the aperture stop 16 corresponding to

an in-focus location of the illuminated line S. The in-focus location is typically characterized by a substantially flat-shaped wave front W_1 .

Fig. 3b illustrates a wave front W_2 of the returned light 28 corresponding to an out-of-focus location of the illuminated line S. The out-of-focus location is characterized by a substantially spherical wave front W_2 . The returned light 28 propagates within regions R_1 and R_2 , which lie substantially far from and close to the optical axis OA_1 , respectively, i.e., periphery and paraxial regions, respectively, with respect to the optical axis OA_1 . Significant curvatures of the wave front W_2 are located within the periphery regions R_1 , while being relatively negligible within the paraxial regions R_2 . The periphery regions of the lens are more sensitive to an out-of-focus position of the light source. Therefore, detected light formed by light components propagating within the periphery regions R_1 contains the main information indicative of the out-of-focus location of the line S. This is associated with the principles of light propagation through a lens: with respect to rays coming from the same point on the optical axis of the lens and impinging on the lens at different distances from the optical axis, the further a ray emerges from the optical axis of the lens, the more strongly it is refracted.

It should be understood that since the light beams coming from spaced-apart locations on the optical axis (i.e. before-focus, in-focus and after-focus) impinge onto the same location on the lens at different angles, these beams are differently refracted by the focusing lens. The slits are located so as to pick up the light components propagating within the paraxial and periphery regions of the optical axis. Therefore, a certain phase difference exists between the light emerging respectively from the slits 35a and 35b, as well as between the light emerging respectively from the slits 35c and 35b. The optics 30

creates a magnified image of the aperture stop 16 in the slits' plane CP_1 . To this end, the short slits 35a and 35c are provided at those locations on the plate 35 that interact with the light components representative of the magnified images of the regions R_1 (in accordance with the known image magnification produced by the lens arrangement 30).

5 Since the width of the slits is very small (about $5\mu\text{m}$), the light ensuing from the slits will be diffracted in the Y-direction. Light components ensuing from the upper slit 35a and from the respective half of the central slit 35c will interfere on the sensing surface 21 of the CCD, and will produce an interference pattern IM_1 . Similarly, light ensuing from the lower slit 35c and from the other half of the central slit 35b will
10 interfere and produce an interference pattern IM_2 .

Thus, two images IM_1 and IM_2 are obtained on the sensing surface 21 of the CCD camera, actuating corresponding sensing elements, each representing a pixel of the image. Each of the images is the interference pattern formed by interference of the light components picked up by the corresponding short slit and the half of the central slit.

15 Owing to the above design of the optical system 9 and the appropriate accommodation of the sensing surface 21, each of the finally obtained images IM_1 and IM_2 contains information indicative of the image of the aperture stop 16 formed by the light component propagating within a corresponding one of the periphery regions R_1 ; the image of the scan line S along the Z-axis; the image of the corresponding interference
20 pattern along the X-axis; and the phase difference between the light components forming this interference pattern.

Figs. 4, 5a-5b, and 6a-6b illustrate in-focus and two out-of-focus situations as detected by the CCD 20. Fig. 4 shows the entire image IM formed of two image-parts

IM₁ and IM₂. Each of the image-parts is the interference pattern, i.e., an array of "dark" and "light" fringes. The two images IM₁ and IM₂ are displaced with respect to each other only along the X-axis, namely, each two "dark" fringes $F^{(d)}_1$ and $F^{(d)}_2$ (corresponding to the maximum intensity of the output signal) in the two patterns IM₁ and IM₂, respectively, are aligned in a line 46a, and each two "light" fringes $F^{(l)}_1$ and $F^{(l)}_2$ (corresponding to the minimum intensity of the output signal) in the two patterns are aligned in a line 46b. This relative position of the image-parts IM₁ and IM₂ corresponds to the desired in-focus position of the wafer's surface 2a, the so-called "best focus". Before the detection procedure begins, the "best focus" should be found.

10 Figs. 5a and 5b illustrate, respectively, the entire image IM⁽¹⁾ formed by two image-parts IM₁ and IM₂, and graph G₁⁽¹⁾ and G₂⁽¹⁾ representative of the corresponding output signal of the CCD. This situation corresponds to one out-of-focus position of the wafer's surface 2a (e.g., after-focus position). As shown in Fig. 5a, when the wafer moves out of focus in one direction, the image-parts IM₁ and IM₂ displace in two opposite
15 directions D₁ and D₂, respectively, being spaced from each other in the X- and Y-axes. Fringes $F^{(d)}_1$ and $F^{(d)}_2$ (and $F^{(l)}_1$ and $F^{(l)}_2$) are displaced from each other a certain distance. This displacement occurs because the light beams returned from the wafer now impinge onto the focusing/collecting lens at different angles (as compared to the situation of Fig. 4), and are therefore differently refracted by the lens. The angles of incidence of the
20 beams onto the slits' plane define the intensity pattern structure in the output interference patterns.

The sensing elements of the CCD camera 20 operate in a conventional manner to produce electrical signals in response to the sensed light and to transmit the electrical

signals to the output circuit 22. In Fig. 5b, curves $G_1^{(1)}$ and $G_2^{(1)}$ represent the intensity distribution of the output signal corresponding to the image parts IM_1 and IM_2 , respectively. As shown, a certain phase difference exists between the two output signals. Since the phase difference can be estimated very accurately, the technique of the present invention enables very accurate estimation of the focus error.

Thus, the processor 24 analyzes the output signals coming from the detector 20 and generates the focus correction signal, optionally, concurrently presenting the entire image $IM^{(1)}$ on the display 26. In response to the focus correction signal, the servomotor 18 operates accordingly to provide the necessary displacement of the wafer 2 with respect to the focal plane of the objective lens 16.

Figs. 6a and 6b illustrate, respectively, the entire image $IM^{(2)}$ formed by two image-parts IM_1 and IM_2 , and graphs $G_1^{(2)}$ and $G_2^{(2)}$ representative of the corresponding output signal of the CCD. This situation corresponds to another out-of-focus position of the wafer's surface 2a (e.g., before-focus position). As shown in Fig. 6a, when the wafer moves out of focus in the other opposite direction, the image-parts IM_1 and IM_2 displace in the directions D_2 and D_1 , respectively.

The apparatus 1a is tested before the detection procedure. That is, a so-called learning mode is applied in order to detect which one of the situations shown in Figs. 5a-5b and 6a-6b corresponds to the "before-focus" location, and which one corresponds to the "after-focus" location of the surface 2a.

It should be noted that the technique of the present invention actually presents dynamic auto-focusing, namely, the auto-focus detection should preferably be performed continuously during the processing of an article (e.g., inspection of wafers). When the

upper and lower slits 35a and 35c are placed so as to pick up the light components propagating substantially at the edges of the aperture stop 16, one depth-of-focus error gives a $\pi/2$ phase shift of the fringes $F^{(d)}_1$ and $F^{(d)}_2$ (and $F^{(l)}_1$ and $F^{(l)}_2$).

The calculation of the light intensity on the CCD plane will now be explained with reference to Fig. 7 showing schematically the light propagation through the optical system 9. In the figure:

- r_1 and r_2 are the lengths of the optical paths passed by two collected light components 28b and 28a, which emerge from the central slits 35b and the upper short slit 35a, respectively, and interact in the CCD plane CP_2 to form the fringe of the interference pattern IM_1 ;
- r'_1 and r'_2 are the lengths of the optical paths passed by two collected light components 28b and 28c, which emerge from the central slit 35b and the lower short slit 35c, respectively, and interact in the CCD plane CP_2 to form the fringe of the interference pattern IM_2 ;
- d is the distance (along the Y-axis) between the central long slit 35b and each of the short slits 35a and 35c;
- L is the distance (along the Z-axis) between the blocking plate 35 and the CCD plane CP_2 , and
- δ is the defocus (i.e., the distance between the current location of the wafer and the focal plane P).

If $I_1(y)$ is the intensity of the interference pattern formed by light emitted from the central slit 35b and light emitted from the upper short slit 35a, and $I_2(y)$ is the intensity of

the interference pattern formed by light emitted from the central slit 35b and light emitted from the lower short slit 35c, these intensities as functions of the defocus δ are as follows:

$$I_1(y) = \left| A \cdot \cos \left(\left(\frac{2\pi}{\lambda} (|r_1| - |r_2| - \Delta) \right) \right) \right|^2$$

$$I_2(y) = \left| A \cdot \cos \left(\left(\frac{2\pi}{\lambda} (|r'_1| - |r'_2| - \Delta) \right) \right) \right|^2$$

5 Using simple geometry, the argument of the cos-function can be approximated as follows:

$$|r_1| - |r_2| = L \cdot \left[\sqrt{1 + \left(\frac{y}{L} \right)^2} - \sqrt{1 + \left(\frac{y-d}{L} \right)^2} \right] \cong \frac{d}{L} \left(y - \frac{d}{2} \right)$$

$$|r'_1| - |r'_2| = L \cdot \left[\sqrt{1 + \left(\frac{y}{L} \right)^2} - \sqrt{1 + \left(\frac{y+d}{L} \right)^2} \right] \cong \frac{d}{L} \left(-y - \frac{d}{2} \right)$$

Using the principles of geometrical optics, $\Delta(\delta)$ may be approximated as follows:

$$10 \quad \Delta = R - \sqrt{R^2 + d^2} \cong \frac{1}{2} \cdot \frac{d^2}{R}$$

wherein:

$$\frac{1}{f} = \frac{1}{f+d} + \frac{1}{R}; \Rightarrow R \cong \frac{f^2}{\delta}; \Rightarrow \Delta \cong \frac{1}{2} \cdot \frac{d^2}{f^2} \cdot \delta$$
 In view of the above, the intensity

profiles as functions of defocus in two images IM₁ and IM₂ are as follows:

$$I_1(y, \delta) = \left| A \cdot \cos \left(\frac{2\pi}{\lambda} \cdot \left[\frac{d}{L} \left(\frac{d}{2} - y \right) + \frac{1}{2} \cdot \frac{d^2}{f^2} \cdot \delta \right] \right) \right|^2$$

$$15 \quad I_2(y, \delta) = \left| A \cdot \cos \left(\frac{2\pi}{\lambda} \cdot \left[\frac{d}{L} \left(\frac{d}{2} + y \right) + \frac{1}{2} \cdot \frac{d^2}{f^2} \cdot \delta \right] \right) \right|^2$$

Thus, the relation between the two intensity profiles as measured on the CCD enables determination of the position of the wafer 2 relative to the focal plane P (i.e., the defocus δ).

Figs. 8a-8b and 9a-9b illustrate two possible examples, respectively, of the slits' arrangement within the blocking plate, aimed at extending the dynamic range of the detected signals. In both examples, the so-called "double slit" arrangement is used, i.e., two pairs of "short slits" are provided in a blocking plate at opposite sides, respectively, of a central "long" slit.

As shown in Fig. 8a, a blocking plate 135 (to be accommodated in the optical path of light entering the optical system 9) is formed with a central long slit 135b, and two pairs of short slits 135a'-135a'' and 135c'-135c''. The slits all are arranged so that they are in a spaced-apart parallel relationship along the Y-axis, and the two pairs of short slits, as well as the short slits within each pair, are spaced with respect to each other along both the Y- and the X-axes. Fig. 8b illustrates an image IM (as obtained on the CCD) composed of four patterns (image parts) IM₁-IM₄. The interference patterns IM₁ and IM₂ are formed by interference between the light components ensuing from the central slit 135b and each of the inner slits 135a' and 135c', respectively. The interference patterns IM₃ and IM₄ are formed by interference between the light emitted from the central slit 135b, and each of the outer slits 135a'' and 135c'', respectively. As shown, the inner slits 135a' and 135c' provide high sensitivity patterns and low dynamic range, and the outer slits 135a'' and 135c'' provide low sensitivity patterns and large dynamic range.

In the example of Figs. 9a-9b, a blocking plate 235, similar to the above-described example, is formed with a central long slit 235b, and two pairs of short slits 235a'-235a''

and 235c'-235c''. Here, as distinguished from the previous example, the two short slits of each pair are spaced with respect to each other only along the Y-axis. The provision of inner slits 235a' and 235c, and outer slits 235a'' and 235c'' provide a similar result: a high spatial frequency pattern with low resolution and large dynamic range, and a low spatial frequency pattern with low resolution and large dynamic range. However, as shown in Fig. 9b, each of the two image parts (interference pattern) IM₁ and IM₂ is a superposition of two images produced by light components ensuing from the slits 235a' and 235a' (and 235c' and 235c'').

Those skilled in the art will readily appreciate that various modifications and changes may be applied to the preferred embodiments of the invention as hereinbefore exemplified without departing from its scope as defined in and by the appended claims. For example, the article to be maintained at a desired position may be an information carrier, and the surface to be maintained in the focal plane may be that defined by an addressed information layer.